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The difference in densily between pure water and $\mathrm{CaCl}_{2}(\mathrm{aq})$ has been measured with a vibrating tube densimeter at molalities from 0.05 to $6.4 \mathrm{~mol} \mathrm{~kg}^{-1}$, temperatures from 323 to $\mathbf{6 0 0 ~ K}$, and pressures up to $\mathbf{4 0}$ MPa . The results were fitted to a cuble spline surface in three dimensions ( $P, T$, and $m$ ). The data extend the range of experimental data for $\mathrm{CaCl}_{2}(\mathrm{aq})$ to 600 K .

## Introduction

As part of a continuing investigation of the thermodynamic properties of aqueous solutions at high temperatures, a densimeter based on the vibrating tube principle was recently constructed in our laboratory (1). The densimeter has previously been used to measure densities of aqueous $\mathrm{NaCl}, \mathrm{KCl}$, $\mathrm{NaBr}, \mathrm{LiCl}, \mathrm{MgCl}_{2}$, and $\mathrm{CaCl}_{2}$ at 298.15 K and pressures up to 40 MPa (2). In this paper, we present measurements of the densities of aqueous $\mathrm{CaCl}_{2}$ at temperatures from 323 to 600 $K$ and pressures up to 40 MPa .

## Experimental Section

The densimeter has been described in detail elsewhere (1-3). It is a vibrating U-tube type densimeter which is used to measure the differences in density between an aqueous solution and pure water at a given temperature and pressure. In this experiment, the change in density $\Delta d$ is given by

$$
\begin{equation*}
\Delta d=d-d_{0}=K\left(\tau^{2}-\tau_{0}^{2}\right) \tag{1}
\end{equation*}
$$

where the subscript o refers to pure water (the reference fluid), $\tau$ is the period of vibration of the $U$ tube, and $K$ is a calibration constant determined at each temperature. In a typical experiment degassed, distilled deionized water was pumped through the densimeter at $0.75 \mathrm{~cm}^{3} \mathrm{~min}^{-1}$ to establish a reference base line. A Rheodyne 7010 HPLC injection valve was employed to introduce a $6-\mathrm{mL}$ sample of solution into the flowing stream. As the sample passed through the instrument, a sample plateau was measured, which was followed by a return to the water base line. The average of the two water base lines was used in calculating the density differences. The temperature of the densimeter block was maintained constant to 0.001 K and was measured by a Burns Engineering platinum resistance thermometer, Model XPPOG5-2-5B, and an ESI Model PVD300 Kelvin bridge with a rated accuracy of $0.02 \%$. The accuracy of the temperature measured in this fashion was estimated to be $\pm 0.08 \mathrm{~K}$ at 300 K and $\pm 0.3 \mathrm{~K}$ at 600 K . The system pressure was maintained with a Circle Seal BPR21 series back-pressure regulator and monitored with an in-line McDaniel $0.25 \%$ test gauge with an accuracy of 0.3 MPa .

At each temperature, the system was calibrated with water and nitrogen (1). Since the dependence of the calibration constant on pressure has previously been shown to be negli-

[^0]gible (1), calibrations were performed with nitrogen at low pressure and water at high pressure.

Solutions were prepared with Fisher Scientific Co. ACScertified calcium chloride dihydrate, lot no. 730805. A stock solution was prepared from which all final solutions were prepared by careful mass dilutions. The stock solution was determined gravimetrically to $0.2 \%$. As a check, the densities of the $\mathrm{CaCl}_{2}$ solutions were measured at 298.15 K and atmospheric pressure. The molalities calculated from the densities given by Perron, Roux, and Desnoyers (4) agreed within 0.2\%.

## Results and Discussion

Table I gives the results of the present measurements of relative densities. The precision of the experiments estimated by the reproducibility of the duplicate measurement is better than $0.050 \mathrm{~kg} \mathrm{~m}^{-3}$ at 450 K and below. At 550 K the precision is somewhat worse, and at 600 K the precision is much worse. At 600 K the densimeter block temperature was perturbed by the most concentrated $\mathrm{CaCl}_{2}$ solutions. The perturbations became so dramatic at the highest pressure that the runs could not be performed. Upon cooling, a small leak was discovered near the heat exchanger. Such a leak could explain the problem of block control since the heat of vaporization of pure water and concentrated $\mathrm{CaCl}_{2}(\mathrm{aq})$ are quite different. Although the precision of the low concentration $\mathrm{CaCl}_{2}$ data seem to be unaffected by the leak, the accuracy of the $\mathrm{CaCl}_{2}$ data should be considered to be on the order of $1.0 \mathrm{~kg} \mathrm{~m}^{-3}$ at 600 K and 38 MPa .
The values of $\Delta d$ in Table I were fit to a three-dimensional cubic spline surface in the same way that we have previously fit a three-dimensional apparent molar heat capacity surface in three dimensions $(3,5)$. The knot values and positions for the cubic spline surface of $\Delta \mathrm{d}$ are given in Table II. From these knot values, successive spline interpolation in each of the three dimensions ( $m, T$, and $P$ ) gives the value of $\Delta d$ at any $T, P$, and $m$ within the range of the experimental data. The values of the knots in Table II were found by using a nonlinear least-squares routine to adjust the knots to the values giving a minimum in the sum of the squares of the differences between the calculated and experimental values of $\Delta d$. At zero molality $\Delta d$ was constrained to be zero and the second derivative end conditions were also varied in order to give a minimum in the sum of the squares of the errors. The end conditions are also given in Table II. It was found that the concentration dependence could be represented by four knots at $0,0.1,1.5$, and $6.45 \mathrm{~mol} \mathrm{~kg}^{-1}$, together with a second derivative end condltion at the most concentrated knot. Increasing the number of concentration knots did not significantly improve the fit.

The temperature dependence was found to be adequately represented by four equally spaced knots with second derivative end conditions included. The data of Gates and Wood (2) at 298 K were included in the fit to extend the low-temperature range. The pressure dependence was represented by just two knots, implying a linear pressure dependence. This assumption of linearity in pressure is accurate below 500 K . However, at $550 \mathrm{~K}, \Delta d$ for $\mathrm{CaCl}_{2}$ exhibits a noticeable curvature versus pressure, and errors on the order of $0.8 \mathrm{~kg} \mathrm{~m}^{-3}$ occur as seen

Table I. Values of the Difference in Density, $\Delta d$, for Aqueous $\mathrm{CaCl}_{2}$ at Various Temperatures, Pressures, and Molalities

| $P / \mathrm{MPa}$ | $m /\left(\mathrm{mol} \mathrm{kg}^{-1}\right)$ | $\Delta d /\left(\mathrm{kg} \mathrm{m}^{-3}\right)$ | $\delta^{a} /\left(\mathrm{kg} \mathrm{m}^{-3}\right)$ | $P / \mathrm{MPa}$ | $m /\left(\mathrm{mol} \mathrm{kg}{ }^{-1}\right)$ | $\Delta d /\left(\mathrm{kg} \mathrm{m}^{-3}\right)$ | $\delta^{a} /\left(\mathbf{k g ~ m}^{-3}\right)$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $T=323.16 \mathrm{~K}$ |  |  |  |  |  |  |  |
| 0.101 | 6.4244 | 403.17 | 0.058 | 20.370 | 6.4244 | 401.16 | 0.030 |
| 0.101 | 6.4244 | 402.95 | 0.275 | 20.370 | 6.4244 | 401.20 | -0.013 |
| 0.101 | 5.0100 | 338.34 | -0.023 | 20.240 | 5.0100 | 336.37 | 0.087 |
| 0.101 | 5.0100 | 338.38 | $-0.066$ | 20.240 | 5.0100 | 336.37 | 0.083 |
| 0.101 | 3.1970 | 235.47 | 0.247 | 20.240 | 3.1970 | 233.87 | 0.349 |
| 0.101 | 3.1970 | 235.49 | 0.222 | 20.170 | 3.1970 | 233.89 | 0.333 |
| 0.101 | 1.0240 | 85.32 | -0.061 | 20.170 | 1.0240 | 84.58 | 0.000 |
| 0.101 | 1.0240 | 85.27 | -0.061 | 20.240 | 1.0240 | 84.56 | 0.025 |
| 0.101 | 1.0240 | 85.27 | -0.008 | 20.240 | 1.0240 | 84.58 | 0.000 |
| 0.101 | 0.5246 | 44.92 | 0.157 | 20.240 | 0.5246 | 44.52 | 0.172 |
| 0.101 | 0.5246 | 44.89 | 0.179 | 20.170 | 0.5246 | 44.52 | 0.176 |
| 0.101 | 0.2722 | 23.78 | 0.078 | 20.170 | 0.2722 | 23.58 | 0.076 |
| 0.101 | 0.2722 | 23.78 | 0.079 | 20.170 | 0.2722 | 23.58 | 0.076 |
| 0.101 | 0.1014 | 8.98 | 0.019 | 20.170 | 0.1014 | 8.90 | 0.022 |
| 0.101 | 0.1014 | 8.97 | 0.029 | 20.170 | 0.1014 | 8.90 | 0.019 |
| 0.101 | 0.0497 | 4.43 | -0.008 | 20.240 | 0.0497 | 4.42 | $-0.037$ |
| 0.101 | 0.0497 | 4.46 | -0.040 | 20.240 | 0.0497 | 4.41 | -0.029 |
| $T=323.05 \mathrm{~K}$ |  |  |  |  |  |  |  |
| 37.540 | 6.4244 | 399.42 | 0.070 | 37.470 | 0.5246 | 44.25 | 0.111 |
| 37.540 | 6.4244 | 399.42 | 0.070 | 37.470 | 0.5246 | 44.26 | 0.104 |
| 37.540 | 5.0100 | 334.91 | -0.040 | 37.470 | 0.2722 | 23.34 | 0.128 |
| 37.540 | 5.0100 | 334.93 | -0.054 | 37.470 | 0.2722 | 23.43 | 0.042 |
| 37.540 | 3.1970 | 232.58 | 0.356 | 37.470 | 0.1014 | 8.80 | 0.049 |
| 37.470 | 3.1970 | 232.57 | 0.376 | 37.470 | 0.1014 | 8.80 | 0.049 |
| 37.470 | 1.0240 | 84.14 | -0.130 | 37.470 | 0.0497 | 4.35 | -0.003 |
| 37.470 | 1.0240 | 84.08 | -0.078 | 37.470 | 0.0497 | 4.35 | -0.006 |
| $T=349.16 \mathrm{~K}$ |  |  |  |  |  |  |  |
| 1.000 | 6.4244 | 399.39 | -0.024 | 20.310 | 1.0240 | 84.51 | -0.177 |
| 1.000 | 6.4244 | 399.46 | -0.095 | 20.310 | 0.5246 | 44.53 | 0.106 |
| 1.000 | 5.0100 | 335.68 | -0.049 | 20.310 | 0.5246 | 44.64 | -0.005 |
| 1.000 | 5.0100 | 335.66 | -0.031 | 20.310 | 0.2722 | 23.63 | 0.018 |
| 1.000 | 3.1970 | 234.37 | -0.129 | 20.310 | 0.2722 | 23.67 | -0.023 |
| 1.000 | 3.1970 | 234.40 | -0.157 | 20.310 | 0.1014 | 9.06 | -0.132 |
| 1.000 | 1.0240 | 85.27 | -0.288 | 20.310 | 0.1014 | 8.91 | 0.012 |
| 1.000 | 1.0240 | 85.25 | -0.267 | 20.310 | 0.0497 | 4.46 | -0.072 |
| 1.000 | 0.5246 | 44.95 | 0.048 | 39.890 | 6.4244 | 395.60 | 0.080 |
| 1.000 | 0.5246 | 44.95 | 0.052 | 39.890 | 6.4244 | 395.65 | 0.026 |
| 1.000 | 0.2722 | 23.83 | 0.015 | 39.890 | 5.0100 | 332.05 | -0.048 |
| 1.000 | 0.2722 | 23.83 | 0.012 | 39.890 | 5.0100 | 332.05 | -0.048 |
| 1.000 | 0.1014 | 9.02 | -0.024 | 39.820 | 3.1970 | 231.46 | -0.230 |
| 1.000 | 0.1014 | 9.04 | -0.041 | 39.820 | 3.1970 | 231.44 | -0.206 |
| 1.000 | 0.0497 | 4.48 | -0.056 | 39.820 | 1.0240 | 83.90 | -0.223 |
| 1.000 | 0.0497 | 4.46 | -0.039 | 39.820 | 1.0240 | 83.89 | -0.219 |
| 20.370 | 6.4244 | 397.71 | -0.183 | 39.820 | 0.5246 | 44.15 | 0.131 |
| 20.310 | 6.4244 | 397.68 | -0.149 | 39.820 | 0.5246 | 44.14 | 0.134 |
| 20.310 | 5.0100 | 333.95 | -0.126 | 39.750 | 0.2722 | 23.48 | -0.025 |
| 20.310 | 5.0100 | 333.97 | -0.147 | 39.750 | 0.2722 | 23.46 | -0.004 |
| 20.310 | 3.1970 | 232.98 | -0.231 | 39.680 | 0.1014 | 8.82 | 0.032 |
| 20.310 | 3.1970 | 232.95 | -0.210 | 39.680 | 0.0497 | 4.44 | -0.095 |
| 20.310 | 1.0240 | 84.50 | -0.162 |  |  |  |  |
| $T=399.85 \mathrm{~K}$ |  |  |  |  |  |  |  |
| 1.690 | 6.4244 | 402.74 | -0.043 | 20.370 | 1.0240 | 87.11 | 0.077 |
| 1.690 | 6.4244 | 402.57 | 0.128 | 20.310 | 1.0240 | 87.01 | 0.180 |
| 1.690 | 6.4244 | 402.77 | -0.075 | 20.370 | 0.5246 | 46.19 | 0.067 |
| 1.690 | 5.0100 | 339.46 | -0.019 | 20.370 | 0.5246 | 46.15 | 0.105 |
| 1.690 | 5.0100 | 339.49 | -0.047 | 20.370 | 0.2714 | 24.53 | -0.069 |
| 1.690 | 3.1970 | 239.23 | 0.048 | 20.440 | 0.2714 | 24.58 | -0.118 |
| 1.690 | 3.1970 | 239.21 | 0.069 | 20.310 | 0.1014 | 9.37 | -0.102 |
| 1.690 | 1.0240 | 88.21 | 0.004 | 20.370 | 0.1014 | 9.28 | -0.019 |
| 1.690 | 1.0240 | 88.22 | -0.006 | 20.370 | 0.0497 | 4.64 | -0.092 |
| 1.690 | 0.5246 | 46.75 | 0.094 | 20.310 | 0.0497 | 4.66 | -0.112 |
| 1.690 | 0.5246 | 46.65 | 0.191 | 40.160 | 6.4244 | 397.12 | -0.042 |
| 1.690 | 0.2714 | 24.89 | -0.117 | 40.160 | 6.4244 | 397.12 | -0.050 |
| 1.690 | 0.2714 | 24.92 | -0.148 | 40.300 | 5.0100 | 334.32 | -0.093 |
| 1.690 | 0.1014 | 9.29 | 0.093 | 40.230 | 5.0100 | 334.13 | 0.110 |
| 1.690 | 0.1014 | 9.43 | -0.042 | 40.370 | 5.0100 | 334.24 | -0.023 |
| 1.690 | 0.0497 | 4.45 | 0.163 | 40.440 | 3.1970 | 234.82 | 0.006 |
| 1.690 | 0.0497 | 4.69 | -0.078 | 40.370 | 3.1970 | 234.75 | 0.090 |
| 20.170 | 6.4244 | 399.79 | 0.202 | 40.030 | 1.0240 | 86.03 | 0.071 |
| 20.170 | 6.4244 | 399.98 | 0.018 | 40.100 | 1.0240 | 86.09 | 0.008 |
| 20.370 | 5.0100 | 336.73 | 0.185 | 40.160 | 0.5246 | 45.56 | 0.080 |
| 20.370 | 5.0100 | 336.85 | 0.073 | 40.300 | 0.5246 | 45.53 | 0.111 |
| 20.370 | 3.1970 | 237.03 | 0.107 | 40.370 | 0.2714 | 24.23 | -0.109 |
| 20.370 | 3.1970 | 236.98 | 0.151 | 40.510 | 0.2714 | 24.24 | -0.121 |

Table I (Continued)

| $P / \mathrm{MPa}$ | $m /\left(\mathrm{mol} \mathrm{kg}{ }^{-1}\right)$ | $\Delta d /\left(\mathrm{kg} \mathrm{m}^{-3}\right)$ | $\delta^{a} /\left(\mathrm{kg} \mathrm{m}^{-3}\right)$ | $P / \mathrm{MPa}$ | $m /\left(\mathrm{mol} \mathrm{kg}{ }^{-1}\right)$ | $\Delta d /\left(\mathrm{kg} \mathrm{m}{ }^{-3}\right)$ | $\delta^{a} /\left(\mathrm{kg} \mathrm{m}^{-3}\right)$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 40.580 | 0.1014 | 9.29 | $\bigcirc 0.155$ | 40.640 | 0.0497 | 4.60 | -0.112 |
| 40.640 | 0.1014 | 9.21 | $-0.077$ | 40.710 | 0.0497 | 4.58 | -0.099 |
| $T=450.13 \mathrm{~K}$ |  |  |  |  |  |  |  |
| 3.550 | 6.4244 | 415.01 | 0.029 | 3.480 | 0.2722 | 26.92 | -0.070 |
| 3.550 | 6.4244 | 415.06 | -0.019 | 3.410 | 0.1014 | 10.33 | -0.156 |
| 3.550 | 6.4244 | 415.08 | -0.037 | 3.410 | 0.1014 | 10.32 | -0.152 |
| 3.550 | 5.0100 | 351.05 | -0.088 | 3.410 | 0.0497 | 5.16 | -0.162 |
| 3.550 | 5.0100 | 351.05 | $-0.087$ | 3.410 | 0.0497 | 5.15 | -0.155 |
| 3.550 | 5.0100 | 351.11 | $-0.148$ | 11.340 | 5.0100 | 349.13 | 0.215 |
| 3.550 | 3.1970 | 249.94 | 0.045 | 11.340 | 5.0100 | 349.21 | 0.139 |
| 3.550 | 3.1970 | 249.97 | 0.015 | 11.340 | 1.0240 | 93.14 | -0.062 |
| 3.550 | 1.0240 | 93.90 | $-0.170$ | 11.340 | 1.0240 | 93.11 | -0.035 |
| 3.550 | 1.0240 | 93.89 | -0.159 | 11.270 | 0.2722 | 26.66 | 0.004 |
| 3.480 | 0.5246 | 50.20 | 0.222 | 11.270 | 0.2722 | 26.67 | -0.005 |
| 3.480 | 0.5246 | 50.18 | 0.243 | 20.310 | 6.4244 | 411.07 | -0.031 |
| 3.480 | 0.2722 | 26.88 | -0.026 | 20.310 | 6.4244 | 410.53 | 0.502 |
| $T=449.75 \mathrm{~K}$ |  |  |  |  |  |  |  |
| 20.310 | 6.4244 | 411.14 | -0.223 | 20.440 | 0.1014 | 10.12 | -0.119 |
| 20.310 | 6.4244 | 411.10 | $-0.183$ | 20.440 | 0.1014 | 10.18 | -0.174 |
| 20.310 | 5.0100 | 347.45 | -0.071 | 20.440 | 0.0497 | 5.01 | -0.092 |
| 20.310 | 5.0100 | 347.45 | -0.067 | 20.440 | 0.0497 | 5.05 | -0.130 |
| 20.310 | 3.1970 | 246.86 | 0.077 | 29.130 | 1.0240 | 91.69 | -0.148 |
| 20.310 | 3.1970 | 246.85 | 0.088 | 29.130 | 1.0240 | 91.70 | -0.159 |
| 20.310 | 1.0240 | 92.44 | -0.166 | 29.060 | 5.0100 | 345.68 | -0.092 |
| 20.310 | 1.0240 | 92.43 | -0.152 | 29.060 | 5.0100 | 345.68 | -0.094 |
| 20.310 | 0.5246 | 49.31 | 0.301 | 29.060 | 0.2722 | 26.11 | 0.098 |
| 20.310 | 0.5246 | 49.29 | 0.324 | 29.060 | 0.2722 | 26.07 | 0.132 |
| 20.440 | 0.2722 | 26.40 | 0.016 | 38.160 | 6.4244 | 406.67 | -0.005 |
| 20.440 | 0.2722 | 26.35 | 0.070 |  |  |  |  |
| $T=548.05 \mathrm{~K}$ |  |  |  |  |  |  |  |
| 10.860 | 0.0497 | 7.22 | -0.722 | 24.720 | 3.1970 | 282.79 | 0.650 |
| 10.860 | 0.0497 | 7.28 | -0.784 | 24.720 | 3.1970 | 282.67 | 0.767 |
| 10.860 | 0.1014 | 13.95 | -0.748 | 24.720 | 5.0100 | 390.98 | 1.067 |
| 10.860 | 0.1014 | 13.92 | -0.725 | 24.720 | 5.0100 | 391.04 | 1.005 |
| 10.860 | 0.2722 | 35.06 | -0.539 | 24.720 | 1.0240 | 110.62 | 0.851 |
| 10.860 | 0.2722 | 35.07 | -0.546 | 24.720 | 6.4244 | 460.06 | 0.463 |
| 10.860 | 0.5246 | 63.83 | 0.032 | 24.720 | 6.4244 | 459.54 | 0.991 |
| 10.860 | 0.5246 | 63.84 | 0.025 | 24.720 | 5.0100 | 391.10 | 0.941 |
| 10.790 | 1.0240 | 116.06 | 0.187 | 37.060 | 0.0497 | 6.20 | -0.330 |
| 10.860 | 1.0240 | 116.11 | 0.116 | 37.060 | 0.0497 | 6.24 | -0.373 |
| 10.790 | 3.1970 | 292.92 | -0.682 | 37.060 | 0.1014 | 12.44 | $-0.516$ |
| 10.860 | 3.1970 | 292.93 | -0.736 | 37.060 | 0.1014 | 12.50 | -0.582 |
| 10.860 | 5.0100 | 403.23 | -0.930 | 37.060 | 0.2722 | 31.71 | -0.404 |
| 10.860 | 6.4244 | 471.94 | -0.846 | 37.060 | 0.2722 | 31.73 | -0.423 |
| 24.650 | 0.0497 | 6.62 | -0.453 | 37.060 | 0.5246 | 58.29 | -0.018 |
| 24.650 | 0.0497 | 6.57 | -0.408 | 37.060 | 0.5246 | 58.30 | -0.021 |
| 24.720 | 0.1014 | 12.93 | -0.407 | 37.060 | 1.0240 | 107.20 | 0.032 |
| 24.720 | 0.1014 | 12.93 | -0.410 | 37.060 | 1.0240 | 107.39 | -0.156 |
| 24.720 | 0.2722 | 33.03 | -0.210 | 37.400 | 3.1970 | 276.01 | -0.581 |
| 24.720 | 0.2722 | 33.03 | -0.213 | 37.400 | 3.1970 | 276.15 | -0.723 |
| 24.720 | 0.5246 | 60.42 | 0.483 | 37.400 | 5.0100 | 383.36 | -0.697 |
| 24.720 | 0.5246 | 60.50 | 0.405 | 37.400 | 5.0100 | 383.19 | -0.530 |
| 24.720 | 1.0240 | 111.01 | 0.461 | 37.400 | 6.4244 | 451.44 | -0.585 |
| 24.720 | 1.0240 | 110.89 | 0.576 | 37.400 | 6.4244 | 451.15 | -0.287 |
| $T=597.45 \mathrm{~K}$ |  |  |  |  |  |  |  |
| 20.650 | 0.0151 | 3.19 | -0.805 | 20.650 | 6.4244 | 519.22 | -0.448 |
| 20.650 | 0.0151 | 3.14 | $-0.760$ | 20.650 | 6.4244 | 518.49 | 0.289 |
| 20.650 | 0.0497 | 8.69 | -0.868 | 38.780 | 0.0151 | 2.42 | -0.251 |
| 20.650 | 0.0497 | 8.60 | $-0.777$ | 38.780 | 0.0151 | 2.36 | -0.192 |
| 20.650 | 0.1014 | 16.77 | -0.890 | 38.780 | 0.0497 | 7.36 | -0.250 |
| 20.650 | 0.1014 | 16.75 | -0.871 | 38.780 | 0.0497 | 7.39 | -0.276 |
| 20.650 | 0.2722 | 41.84 | -0.570 | 38.780 | 0.1014 | 14.64 | -0.253 |
| 20.650 | 0.2722 | 41.92 | -0.648 | 38.780 | 0.1014 | 14.53 | -0.143 |
| 20.650 | 0.5246 | 75.50 | 0.101 | 38.850 | 0.2722 | 36.70 | 0.126 |
| 20.650 | 0.5246 | 75.42 | 0.181 | 38.850 | 0.2722 | 36.62 | 0.204 |
| 20.650 | 1.0240 | 134.61 | 0.527 | 38.920 | 0.5246 | 66.32 | 0.042 |
| 20.650 | 1.0240 | 134.33 | 0.805 | 38.920 | 0.5246 | 66.39 | $-0.030$ |
| 20.650 | 3.1970 | 329.55 | -1.028 | 38.920 | 1.0240 | 120.32 | -0.068 |
| 20.650 | 3.1970 | 328.29 | 0.227 | 38.920 | 1.0240 | 120.11 | 0.138 |
| 20.650 | 5.0100 | 447.28 | -0.264 | 38.920 | 1.0240 | 120.34 | -0.091 |
| 20.650 | 5.0100 | 446.22 | 0.800 |  |  |  |  |

$\sigma^{\sigma} \delta$ is the $\Delta d$ calculated by cubic spline interpolation of the knots and end conditions in Table II minus the experimental $\Delta d$.

Table II. Knot Positions and Knot Values for the Cubic Spline Representation of $\Delta d /\left(\mathbf{k g} \mathbf{m}^{-3}\right)$ as a Function of $T$, $P$, and $\boldsymbol{m}^{a}$

| $m /\left(\mathrm{mol} \mathrm{kg}{ }^{-1}\right)$ | $b$ | $T=298.15 \mathrm{~K}$ | $T=400.00 \mathrm{~K}$ | $T=500.00 \mathrm{~K}$ | $T=600.00 \mathrm{~K}$ | $b$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $P=20.0 \mathrm{MPa}$ |  |  |  |  |  |  |
| 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 0.1000 | 1.7 | 8.904 | 9.141 | 10.988 | 15.938 | 11.3 |
| 1.5000 | 43.2 | 122.305 | 122.823 | 140.370 | 185.180 | 85.4 |
| 6.4500 | 79.4 | 410.072 | 401.069 | 432.696 | $525.951^{\text {c }}$ | 149.5 |
| $d$ |  | -5.94 | -5.95 | -5.34 | 3.43 |  |
| $P=40.0 \mathrm{MPa}$ |  |  |  |  |  |  |
| 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 0.1000 | 0.6 | 8.768 | 9.011 | 10.569 | 14.294 | 12.3 |
| 1.5000 | 35.9 | 121.089 | 121.362 | 135.734 | $177.966^{\text {c }}$ | 142.2 |
| 6.4500 | 68.3 | 407.377 | 398.138 | 425.948 | $453.164^{\text {c }}$ | -230.1 |
| d |  | -5.42 | -6.02 | 6.64 | -310 |  |

${ }^{a}$ This fit is a representation of 353 data points. The sum of the squares of the residuals is 32.7 , resulting in a standard error of the fit of $0.330 \mathrm{~kg} \mathrm{~m}^{-3}$. The minimum sum of the squares is 2.44 . ${ }^{b}$ These columns contain the second derivative end conditions multiplied by 10000 , $\left(\partial^{2} \Delta d / \partial T^{2}\right) \times 10^{4} \mathrm{~kg} \mathrm{~m}^{-3} \mathrm{~K}^{-2}$. ${ }^{c}$ Since there are no experimental results at 600 K above $3.2 \mathrm{~mol}^{\mathrm{kg}}{ }^{-1}$ at 20 MPa or above $1.0 \mathrm{~mol} \mathrm{~kg}^{-1}$ at 40 MPa , the spline surface is unreliable above these molalities. ${ }^{d}$ These rows give the second derivative end condition at $m=6.450 \mathrm{~mol} \mathrm{~kg}^{-1}$, $\left(\partial^{2} \Delta d / \partial m^{2}\right) \times 10^{4}$.
in Table I. Unfortunately, a measured pressure curvature at one temperature does not justify fitting with a pressure curvature at all temperatures. The data at 600 K were run at only two pressures, and thus, there is no measure of the nonlinearity at this temperature. A better pressure representation will have to await a more detailed study. The cubic spline surface is a representation of 350 data points, and the standard error of the fit is $0.33 \mathrm{~kg} \mathrm{~m}^{-3}$. The standard error of the data below 500 K is $0.16 \mathrm{~kg} \mathrm{~m}^{-3}$. The decrease in the quality of the fit above 500 K is due to the pressure dependence of $\Delta d$, together with the experimental problems at 600 K . Since at 600 K there are no experimental results above $3.2 \mathrm{~mol}_{\mathrm{kg}^{-1}}$ at 20 MPa or above $1.0 \mathrm{~mol} \mathrm{~kg}^{-1}$ at 40 MPa , the spline surface is unreliable above these molalities.
Ellis (6) has measured thermal expansions for aqueous $\mathrm{CaCl}_{2}$ from 323 to 473 K at $0.05-1.0 \mathrm{~mol} \mathrm{~kg}^{-1}$ at 2 MPa . The temperature dependence of Ellis' data is in excellent agreement with that calculated from our spline surface at temperatures up to and including 448 K . At 473 K the density values calculated here are $0.5 \mathrm{~kg} \mathrm{~m}^{-3}$ higher than the values of Ellis at 0.5 and $1.0 \mathrm{~mol} \mathrm{~kg}^{-1}$. This is approximately 3 times the sum of the estimated errors for both data sets. Romankiw and Chou (7) have measured aqueous $\mathrm{CaCl}_{2}$ densities using a vibrating tube densimeter at 298 to 318 K . Their results are not compatible with our measurements. The previous measurements at 298.1 $K$ with this instrument compared well with those of Perron, Roux, and Desnoyers (4). Zhang and Frantz (8) determined homogenization temperatures for synthetic $\mathrm{CaCl}_{2}(\mathrm{aq})$ fluid inclusions at high temperature and pressure. The combination of their data with the previous measurements of Rodnyanskii et al. $(9,10)$ of the density at the saturation pressure allows the calculation of density as a function of $T$ and $P$ from 300 to $700^{\circ} \mathrm{C}$. Using the equations of Zhang and Frantz (there is a misprint in their eq 21) corrected for the expansion of quartz, we can calculate densities at $326.85{ }^{\circ} \mathrm{C}$ for comparison with the present spline surface. The differences are, for $m=0.5$
mol $\mathrm{kg}^{-1},-17$ and $-24 \mathrm{~kg} \mathrm{~m}^{-3}$ at 20 and 40 MPa and, for $m=$ $1.0 \mathrm{~mol} \mathrm{~kg}^{-1}$, +1 and $-9 \mathrm{~kg} \mathrm{~m}^{-3}$ at 20 and 40 MPa . These differences are within the expected accuracy of the saturation density as estimated by Potter and Clyne ( 10 ) $\left( \pm 10 \mathrm{~kg} \mathrm{~m}^{-3}\right.$ from 250 to $300^{\circ} \mathrm{C}$ with larger errors above $300^{\circ} \mathrm{C}$ ).
The data presented here significantly extend the range and quality of volumetric properties of aqueous $\mathrm{CaCl}_{2}$. These data allow the calculation of the pressure dependence of free energies, enthalpies, and heat capacities. The data at 600 K are not as accurate as can be obtained from the present instrumentation.

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