# Density and Apparent Molar Volume of Aqueous CaCl<sub>2</sub> at 323–600 K

# Jeffrey A. Gates<sup>†</sup> and Robert H. Wood\*

Department of Chemistry, University of Delaware, Newark, Delaware 19716

The difference in density between pure water and  $CaCl_2(aq)$  has been measured with a vibrating tube densimeter at moialities from 0.05 to 6.4 moi kg<sup>-1</sup>, temperatures from 323 to 600 K, and pressures up to 40 MPa. The results were fitted to a cubic spline surface in three dimensions (*P*, *T*, and *m*). The data extend the range of experimental data for  $CaCl_2(aq)$  to 600 K.

## Introduction

As part of a continuing investigation of the thermodynamic properties of aqueous solutions at high temperatures, a densimeter based on the vibrating tube principle was recently constructed in our laboratory (1). The densimeter has previously been used to measure densities of aqueous NaCl, KCl, NaBr, LiCl, MgCl<sub>2</sub>, and CaCl<sub>2</sub> at 298.15 K and pressures up to 40 MPa (2). In this paper, we present measurements of the densities of aqueous CaCl<sub>2</sub> at temperatures from 323 to 600 K and pressures up to 40 MPa.

#### **Experimental Section**

The densimeter has been described in detail elsewhere (1-3). It is a vibrating U-tube type densimeter which is used to measure the differences in density between an aqueous solution and pure water at a given temperature and pressure. In this experiment, the change in density  $\Delta d$  is given by

$$\Delta d = d - d_{0} = K(\tau^{2} - \tau_{0}^{2})$$
(1)

where the subscript o refers to pure water (the reference fluid),  $\tau$  is the period of vibration of the U tube, and K is a calibration constant determined at each temperature. In a typical experiment degassed, distilled deionized water was pumped through the densimeter at 0.75 cm<sup>3</sup> min<sup>-1</sup> to establish a reference base line. A Rheodyne 7010 HPLC injection valve was employed to introduce a 6-mL sample of solution into the flowing stream. As the sample passed through the instrument, a sample plateau was measured, which was followed by a return to the water base line. The average of the two water base lines was used in calculating the density differences. The temperature of the densimeter block was maintained constant to 0.001 K and was measured by a Burns Engineering platinum resistance thermometer, Model XPPOG5-2-5B, and an ESI Model PVD300 Kelvin bridge with a rated accuracy of 0.02%. The accuracy of the temperature measured in this fashion was estimated to be  $\pm 0.08$  K at 300 K and  $\pm 0.3$  K at 600 K. The system pressure was maintained with a Circle Seal BPR21 series back-pressure regulator and monitored with an in-line McDaniel 0.25% test gauge with an accuracy of 0.3 MPa.

At each temperature, the system was calibrated with water and nitrogen (1). Since the dependence of the calibration constant on pressure has previously been shown to be negligible (1), calibrations were performed with nitrogen at low pressure and water at high pressure.

Solutions were prepared with Fisher Scientific Co. ACS-certified calcium chloride dihydrate, lot no. 730805. A stock solution was prepared from which all final solutions were prepared by careful mass dilutions. The stock solution was determined gravimetrically to 0.2%. As a check, the densities of the CaCl<sub>2</sub> solutions were measured at 298.15 K and atmospheric pressure. The molalities calculated from the densities given by Perron, Roux, and Desnoyers (4) agreed within 0.2%.

### **Results and Discussion**

Table I gives the results of the present measurements of relative densities. The precision of the experiments estimated by the reproducibility of the duplicate measurement is better than 0.050 kg m<sup>-3</sup> at 450 K and below. At 550 K the precision is somewhat worse, and at 600 K the precision is much worse. At 600 K the densimeter block temperature was perturbed by the most concentrated CaCl<sub>2</sub> solutions. The perturbations became so dramatic at the highest pressure that the runs could not be performed. Upon cooling, a small leak was discovered near the heat exchanger. Such a leak could explain the problem of block control since the heat of vaporization of pure water and concentrated CaCl<sub>2</sub>(ag) are guite different. Although the precision of the low concentration CaCl<sub>2</sub> data seem to be unaffected by the leak, the accuracy of the CaCl<sub>2</sub> data should be considered to be on the order of 1.0 kg m<sup>-3</sup> at 600 K and 38 MPa.

The values of  $\Delta d$  in Table I were fit to a three-dimensional cubic spline surface in the same way that we have previously fit a three-dimensional apparent molar heat capacity surface in three dimensions (3, 5). The knot values and positions for the cubic spline surface of  $\Delta d$  are given in Table II. From these knot values, successive spline interpolation in each of the three dimensions (*m*, *T*, and *P*) gives the value of  $\Delta d$  at any T, P, and m within the range of the experimental data. The values of the knots in Table II were found by using a nonlinear least-squares routine to adjust the knots to the values giving a minimum in the sum of the squares of the differences between the calculated and experimental values of  $\Delta d$ . At zero molality  $\Delta d$  was constrained to be zero and the second derivative end conditions were also varied in order to give a minimum in the sum of the squares of the errors. The end conditions are also given in Table II. It was found that the concentration dependence could be represented by four knots at 0, 0.1, 1.5, and 6.45 mol kg<sup>-1</sup>, together with a second derivative end condition at the most concentrated knot. Increasing the number of concentration knots did not significantly improve the fit.

The temperature dependence was found to be adequately represented by four equally spaced knots with second derivative end conditions included. The data of Gates and Wood (2) at 298 K were included in the fit to extend the low-temperature range. The pressure dependence was represented by just two knots, implying a linear pressure dependence. This assumption of linearity in pressure is accurate below 500 K. However, at 550 K,  $\Delta d$  for CaCl<sub>2</sub> exhibits a noticeable curvature versus pressure, and errors on the order of 0.8 kg m<sup>-3</sup> occur as seen

<sup>&</sup>lt;sup>†</sup>Present address: E. I. du Pont de Nemours and Co., Inc., Wilmington, DE 19898.

<sup>•</sup> To whom correspondence should be addressed.

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P/MP <sub>a</sub>	$m/(mol ka^{-1})$	$\Delta d/(k\sigma m^{-3})$	$\delta^{a}/(k\sigma m^{-3})$	P/MP <sub>a</sub>	$m/(mol k \sigma^{-1})$	$\Delta d / (k \sigma m^{-3})$	$\delta^a/(k\sigma m^{-3})$
. / 1911 8	(mor <b>k</b> R -)	70 (KR III .)	~ / (wR m .)	1/1415.8	m (mor kg )	Lug (Kg III ')	• / ( <b>rg m</b> ·
		100	T = 32	23.16 K	<b>A</b> 1 <b>A</b> 1	101	
0.101	6.4244	403.17	0.058	20.370	6.4244	401.16	0.030
0.101	6.4244	402.95	0.275	20.370	6.4244	401.20	-0.013
0.101	5.0100	338.34	-0.023	20.240	5.0100	336.37	0.087
0.101	5 0100	226.26	-0.066	20.240	5.0100	226.27	0.001
0.101	5.0100	330.30	-0.066	20.240	5.0100	330.37	0.065
0.101	3.1970	235.47	0.247	20.240	3.1970	233.87	0.349
0.101	3.1970	235.49	0.222	20.170	3.1970	233.89	0.333
0.101	1.0240	85.32	-0.061	20.170	1.0240	84.58	0.000
0.101	1.0240	95.97	-0.061	20.210	1.0240	84.56	0.000
0.101	1.0240	00.27	-0.001	20.240	1.0240	04.00	0.020
0.101	1.0240	85.27	-0.008	20.240	1.0240	84.58	0.000
0.101	0.5246	44.92	0.157	20.240	0.5246	44.52	0.172
0.101	0.5246	44.89	0.179	20.170	0.5246	44.52	0.176
0.101	0.0210	00.70	0.079	20.170	0.0799	00 50	0.076
0.101	0.2722	20.70	0.078	20.170	0.2722	20.00	0.070
0.101	0.2722	23.78	0.079	20.170	0.2722	23.58	0.076
0.101	0.1014	8.98	0.019	20.170	0.1014	8.90	0.022
0.101	0.1014	8.97	0.029	20.170	0.1014	8.90	0.019
0 101	0.0497	1 13	-0.008	20.240	0.0497	4 49	-0.037
0.101	0.0497	4.40	-0.008	20.240	0.0497	4.42	-0.001
0.101	0.0497	4.46	-0.040	20.240	0.0497	4.41	-0.029
			T = 32	23.05 K			
97 540	6 4944	300 49	0.070	97 470	0.5246	44 95	0 111
37.040	0.4244	333.42	0.070	57.470	0.5240	44.20	0.111
37.540	6.4244	399.42	0.070	37.470	0.5246	44.26	0.104
37.540	5.0100	334.91	-0.040	37.470	0.2722	23.34	0.128
37.540	5.0100	334.93	-0.054	37.470	0.2722	23.43	0.042
97 540	9 1070	000 50	0.256	97 470	0 1014	9 90	0.040
37.540	3.1970	232.38	0.336	37.470	0.1014	0.00	0.049
37.470	3.1970	232.57	0.376	37.470	0.1014	8.80	0.049
37.470	1.0240	84.14	-0.130	37.470	0.0497	4.35	-0.003
37.470	1.0240	84.08	-0.078	37.470	0.0497	4.35	-0.006
			·				
			T = 34	49.16 K			
1.000	6.4244	399.39	-0.024	20.310	1.0240	84.51	-0.177
1.000	6.4244	399.46	-0.095	20.310	0.5246	44.53	0.106
1 000	5 0100	335.69	-0.049	20.310	0.5946	11 61	-0.005
1.000	5.0100	000.00	-0.043	20.010	0.0240	11.01	-0.000
1.000	5.0100	335.66	-0.031	20.310	0.2722	23.63	0.018
1.000	3.1970	234.37	-0.129	20.310	0.2722	23.67	-0.023
1.000	3.1970	234.40	-0.157	20.310	0.1014	9.06	-0.132
1 000	1 0 2 4 0	85.27	-0.288	20.310	0 1014	8 91	0.012
1.000	1.0240	05.05	0.200	20.010	0.1014	4.46	0.012
1.000	1.0240	85.25	-0.267	20.310	0.0497	4.40	-0.072
1.000	0.5246	44.95	0.048	39.890	6.4244	395.60	0.080
1.000	0.5246	44.95	0.052	39.890	6.4244	395.65	0.026
1 000	0 2722	23 83	0.015	39 890	5 0100	332.05	-0.048
1.000	0.2722	20.00	0.010	00.000	5.0100	002.00	0.040
1.000	0.2722	23.83	0.012	39.890	5.0100	332.05	-0.048
1.000	0.1014	9.02	-0.024	39.820	3.1970	231.46	-0.230
1.000	0.1014	9.04	-0.041	39.820	3.1970	231.44	-0.206
1.000	0.0497	4 4 8	-0.056	39,820	1 0240	83.90	-0 223
1.000	0.0407	4.40	0.000	00.020	1.0240	00.00	0.220
1.000	0.0497	4.40	-0.039	39.020	1.0240	03.09	-0.219
20.370	6.4244	397.71	-0.183	39.820	0.5246	44.15	0.131
20.310	6.4244	397.68	-0.149	39.820	0.5246	44.14	0.134
20.310	5.0100	333.05	-0.126	39 750	0.2722	23.48	-0.025
20.010	5.0100	000.00	0.120	00.700	0.2722	20.40	0.020
20.310	5.0100	333.97	-0.147	39.750	0.2722	23.40	-0.004
20.310	3.1970	232.98	-0.231	39.680	0.1014	8.82	0.032
20.310	3.1970	232.95	-0.210	39.680	0.0497	4.44	-0.095
20.310	1.0240	84.50	-0.162	- *			
			<b>T</b>	0.05 12			
1 000	0.4044	400 E 1	T = 39	99.85 K	1.0040	07 11	0.055
1.690	6.4244	402.74	-0.043	20.370	1.0240	87.11	0.077
1.690	6.4244	402.57	0.128	20.310	1.0240	87.01	0.180
1,690	6.4244	402.77	-0.075	20.370	0.5246	46.19	0.067
1 600	5 0100	330 16	-0.010	20.010	0 5946	46 15	0 105
1.050	5.0100	000.40	-0.015	20.370	0.0240	40.10	0.100
1.690	5.0100	339.49	-0.047	20.370	0.2714	24.53	-0.069
1.690	3.1970	239.23	0.048	20.440	0.2714	24.58	-0.118
1.690	3.1970	239.21	0.069	20.310	0.1014	9.37	-0.102
1 600	1 0940	gg 91	0.004	20.020	0 1014	0.08	_0.010
1.090	1.0240	00.21	0.004	20.370	0.1014	9.40	-0.019
1.690	1.0240	88.22	-0.006	20.370	0.0 <b>49</b> 7	4.64	-0.092
1.690	0.5246	46.75	0.094	20.310	0.0497	4.66	-0.112
1,690	0.5246	46.65	0.191	40,160	6.4244	397.12	-0.042
1 600	0.0214	94 00	-0.117	10.100	6 4944	307 19	0
1.090	0.2714	24.69	-0.117	40.160	0.4244	001.12	-0.000
1.690	0.2714	24.92	-0.148	40.300	5.0100	334.32	-0.093
1.690	0.1014	9.29	0.093	40.230	5.0100	334.13	0.110
1.690	0 1014	9 4 3	-0.042	40 370	5.0100	334.24	-0.023
1 600	0.0407	4 AE	0.169	40.440	9 1070	00100	0.000
1,090	0.0497	4.40	0.103	40.440	3.19/0	204.02	0.000
1.690	0.0497	4.69	-0.078	40.370	3.1970	234.75	0.090
20.170	6.4244	399.79	0.202	40.030	1.0240	86.03	0.071
20,170	6 4244	399.98	0.018	40,100	1.0240	86.09	0.008
20 270	5 0100	296 79	0.195	10.100	A 5940	A5 50	0.000
20.370	5.0100	000.70	0.100	40.100	0.0240	40.00	0.000
20.370	5.0100	336.85	0.073	40.300	0.5246	45.53	0.111
20.370	3.1970	237.03	0.107	40.370	0.2714	24.23	-0.109
20.370	3,1970	236.98	0.151	40.510	0.2714	24.24	-0.121

	P/MPa	$m/(\text{mol kg}^{-1})$	$\Delta d/(\mathrm{kg~m^{-3}})$	$\delta^a/(\mathrm{kg}~\mathrm{m}^{-3})$	P/MPa	$m/(\text{mol kg}^{-1})$	$\Delta d/(\text{kg m}^{-3})$	δ <sup>a</sup> /(kg m <sup>-3</sup> )
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	40.580	0.1014	9.29	-0.155	40.640	0.0497	4.60	-0.112
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	40.640	0.1014	9.21	-0.077	40.710	0.0497	4.58	-0.099
$\begin{array}{cccccccccccccccccccccccccccccccccccc$				au .	- 450 12 K			
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3.550	6.4244	415.01	0.029	- 400.13 K 3 480	0 2722	26.92	-0.070
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3.550	6.4244	415.06	-0.019	3.410	0.1014	10.33	-0.156
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3.550	6.4244	415.08	-0.037	3.410	0.1014	10.32	-0.152
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3.550	5.0100	351.05	-0.088	3.410	0.0497	5.16	-0.162
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3.550	5.0100	351.05	-0.087	3.410	0.0497	5.15	-0.155
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3.550	5.0100	351.11	-0.148	11.340	5.0100	3 <b>49.1</b> 3	0.215
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3.550	3.1970	249.94	0.045	11.340	5.0100	349.21	0.139
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	3.550	3.1970	249.97	0.015	11.340	1.0240	93.14	-0.062
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3.550	1.0240	93.90	-0.170	11.340	1.0240	93.11	-0.035
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3.550	0.5240	93.89 50.90	-0.159	11.270	0.2722	20.00	0.004
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	3 480	0.5246	50.18	0.222	20.310	6 4 9 4 4	411.07	-0.003
$ \begin{array}{c} T = 449.75 \ K \\ \hline T = 549.75 \ K \\ \hline T = 548.55 \ K \\ \hline T = 558.55 \ K \\ \hline T = 557.45 \ K \\ \hline T = 5$	3.480	0.2722	26.88	-0.026	20.310	6.4244	410.53	0.502
$\begin{array}{c c c c c c c c c c c c c c c c c c c $				m				
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	20.210	6 4944	411 14	0.000	= 449.75 K	0 1014	10.10	0.110
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	20.310	6 4244	411.14	-0.223	20.440	0.1014	10.12	-0.119
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	20.310	5 0100	347 45	-0.071	20.440	0.1014	5.01	-0.174
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	20.310	5.0100	347.45	-0.067	20.440	0.0497	5.05	-0.130
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	20.310	3.1970	246.86	0.077	29.130	1.0240	91.69	-0.148
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	20.310	3.1970	246.85	0.088	29.130	1.0240	91.70	-0.159
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	20.310	1.0240	92.44	-0.166	29.060	5.0100	345.68	-0.092
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	20.310	1.0240	92.43	-0.152	29.060	5.0100	345.68	-0.094
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	20.310	0.5246	49.31	0.301	29.060	0.2722	26.11	0.098
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	20.310	0.5246	49.29	0.324	29.060	0.2722	26.07	0.132
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	20.440	0.2722	26.40	0.016	38.160	6.4244	406.67	-0.005
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	20.440	0.2722	20.30	0.070				
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$				T :	= 548.05 K			
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	10.860	0.0497	7.22	-0.722	24.720	3.1970	282.79	0.650
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	10.860	0.0497	7.28	-0.784	24.720	3.1970	282.67	0.767
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	10.860	0.1014	13.95	-0.748	24.720	5.0100	390.98	1.067
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	10.860	0.1014	13.92	-0.725	24.720	5.0100	391.04	1.005
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	10.860	0.2722	35.00	-0.539	24.720	6 4944	460.06	0.601
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	10.860	0.5246	63.83	0.032	24.720	6.4244	459.54	0.991
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	10.860	0.5246	63.84	0.025	24.720	5.0100	391.10	0.941
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	10.790	1.0240	116.06	0.187	37.060	0.0497	6.20	-0.330
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	10.860	1.0240	116.11	0.116	37.060	0.0497	6.24	-0.373
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	10.790	3.1970	292.92	-0.682	37.060	0.1014	12.44	-0.516
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	10.860	3.1970	292.93	-0.736	37.060	0.1014	12.50	-0.582
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	10.860	5.0100	403.23	-0.930	37.060	0.2722	31.71	-0.404
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	24 650	0,4244	4/1.94	-0.846	37.060	0.2722	31.73	-0.423
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	24.050	0.0497	6.57	-0.408	37.060	0.5246	00.29 58 30	-0.018
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	24.720	0.1014	12.93	-0.407	37.060	1.0240	107.20	0.021
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	24.720	0.1014	12.93	-0.410	37.060	1.0240	107.39	-0.156
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	24.720	0.2722	33.03	-0.210	37.400	3.1970	276.01	-0.581
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	24.720	0.2722	33.03	-0.213	37.400	3.1970	276.15	-0.723
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	24.720	0.5246	60.42	0.483	37.400	5.0100	383.36	-0.697
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	24.720	0.5246	60.50	0.405	37.400	5.0100	383.19	-0.530
24.7201.0240110.390.57637.4006.4244451.15 $-0.287$ T = 597.45 K20.6500.01513.19 $-0.805$ 20.6506.4244519.22 $-0.448$ 20.6500.01513.14 $-0.760$ 20.6506.4244518.490.28920.6500.04978.69 $-0.868$ 38.7800.01512.42 $-0.251$ 20.6500.101416.77 $-0.890$ 38.7800.04977.36 $-0.192$ 20.6500.101416.75 $-0.871$ 38.7800.04977.39 $-0.276$ 20.6500.272241.84 $-0.570$ 38.7800.101414.64 $-0.253$ 20.6500.272241.92 $-0.648$ 38.7800.101414.53 $-0.143$ 20.6500.524675.500.10138.8500.272236.620.20420.6501.0240134.610.52738.9200.524666.320.04220.6501.0240134.610.52738.9200.524666.39 $-0.030$ 20.6503.1970329.55 $-1.028$ 38.9201.0240120.32 $-0.068$ 20.6503.1970329.55 $-1.028$ 38.9201.0240120.110.13820.6505.0100447.28 $-0.264$ 38.9201.0240120.34 $-0.091$ 20.6505.0100446.220.800 $-0.264$ $-0.264$ $-0.264$ $-0.291$	24.720	1.0240	111.01	0.461	37.400	6.4244	451.44	-0.585
$T = 597.45 \text{ K}$ $\begin{array}{c ccccccccccccccccccccccccccccccccccc$	24.720	1.0240	110.89	0.576	37.400	6.4244	451.15	-0.287
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$				T :	= 597.45 K			
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	20.650	0.0151	3.19	-0.805	20.650	6.4244	519.22	-0.448
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	20.650	0.0151	3.14	-0.760	20.650	6.4244	518.49	0.289
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	20.650	0.0497	8.60	-0.868	38,780	0.0151	2.42	-0.251
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	20.000	0.1014	16 77	-0.777	30.700	0.0151	2.30 7 36	-0.192
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	20.650	0.1014	16.75	-0.871	38.780	0.0497	7.39	-0.276
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	20.650	0.2722	41.84	-0.570	38.780	0.1014	14.64	-0.253
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	20.650	0.2722	41.92	-0.648	38.780	0.1014	14.53	-0.143
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	20.650	0.5246	75.50	0.101	38.850	0.2722	36.70	0.126
20.650         1.0240         134.61         0.527         38.920         0.5246         66.32         0.042           20.650         1.0240         134.33         0.805         38.920         0.5246         66.39         -0.030           20.650         3.1970         329.55         -1.028         38.920         1.0240         120.32         -0.068           20.650         3.1970         328.29         0.227         38.920         1.0240         120.11         0.138           20.650         5.0100         447.28         -0.264         38.920         1.0240         120.34         -0.091           20.650         5.0100         446.22         0.800	20.650	0.5246	75.42	0.181	38.850	0.2722	36.62	0.204
20.650         1.0240         134.33         0.805         38.920         0.5246         66.39         -0.030           20.650         3.1970         329.55         -1.028         38.920         1.0240         120.32         -0.068           20.650         3.1970         328.29         0.227         38.920         1.0240         120.11         0.138           20.650         5.0100         447.28         -0.264         38.920         1.0240         120.34         -0.091           20.650         5.0100         446.22         0.800         -0.800         -0.091         -0.091	20.650	1.0240	134.61	0.527	38.920	0.5246	66.32	0.042
20.000         5.1970         329.55         -1.028         38.920         1.0240         120.32         -0.068           20.650         3.1970         328.29         0.227         38.920         1.0240         120.11         0.138           20.650         5.0100         447.28         -0.264         38.920         1.0240         120.34         -0.091           20.650         5.0100         446.22         0.800         -0.800         -0.091         -0.091	20.650	1.0240	134.33	0.805	38.920	0.5246	66.39	-0.030
20.650         5.1970         526.25         0.227         58.920         1.0240         120.11         0.138           20.650         5.0100         447.28         -0.264         38.920         1.0240         120.34         -0.091           20.650         5.0100         446.22         0.800         1.0240         120.34         -0.091	20.000 20.650	3.1970	329.55	-1.028	38.920	1.0240	120.32	-0.068
20.650 5.0100 446.22 0.800	20.650	5.0100	320.29 447 98	-0.264	38,920	1.0240	120.11	0.138
	20.650	5.0100	446.22	0.800	00.020	1.0470	120.01	0.001

Table I (Continued)

 $^{a}\delta$  is the  $\Delta d$  calculated by cubic spline interpolation of the knots and end conditions in Table II minus the experimental  $\Delta d$ .

Table II. Knot Positions and Knot Values for the Cubic Spline Representation of  $\Delta d/(\text{kg m}^3)$  as a Function of T, P, and  $m^a$ 

					• /		
 $m/(\text{mol kg}^{-1})$	Ь	T = 298.15  K	T = 400.00  K	T = 500.00  K	T = 600.00  K	Ь	
			P = 20.0  MPa				
0.0	0.0	0.0	0.0	0.0	0.0	0.0	
0.1000	1.7	8.904	9.141	10.988	15.938	11.3	
1.5000	43.2	122.305	122.823	140.370	185,180	85.4	
6.4500	79.4	410.072	401.069	432.696	525.951°	149.5	
d		-5.94	-5.95	-5.34	3.43		
			P = 40.0  MPa				
0.0	0.0	0.0	0.0	0.0	0.0	0.0	
0.1000	0.6	8.768	9.011	10.569	14.294	12.3	
1.5000	35.9	121.089	121.362	135.734	177.966°	142.2	
6.4500	68.3	407.377	398.138	425.948	453.164°	-230.1	
d		-5.42	-6.02	6.64	-310		

<sup>a</sup> This fit is a representation of 353 data points. The sum of the squares of the residuals is 32.7, resulting in a standard error of the fit of 0.330 kg m<sup>-3</sup>. The minimum sum of the squares is 2.44. <sup>b</sup>These columns contain the second derivative end conditions multiplied by 10000,  $(\partial^2 \Delta d/\partial T^2) \times 10^4$  kg m<sup>-3</sup> K<sup>-2</sup>. Since there are no experimental results at 600 K above 3.2 mol kg<sup>-1</sup> at 20 MPa or above 1.0 mol kg<sup>-1</sup> at 40 MPa, the spline surface is unreliable above these molalities. <sup>d</sup> These rows give the second derivative end condition at m = 6.450 mol kg<sup>-1</sup>,  $(\partial^2 \Delta d / \partial m^2) \times 10^4$ .

in Table I. Unfortunately, a measured pressure curvature at one temperature does not justify fitting with a pressure curvature at all temperatures. The data at 600 K were run at only two pressures, and thus, there is no measure of the nonlinearity at this temperature. A better pressure representation will have to await a more detailed study. The cubic spline surface is a representation of 350 data points, and the standard error of the fit is 0.33 kg m<sup>-3</sup>. The standard error of the data below 500 K is 0.16 kg m<sup>-3</sup>. The decrease in the quality of the fit above 500 K is due to the pressure dependence of  $\Delta d$ , together with the experimental problems at 600 K. Since at 600 K there are no experimental results above 3.2 mol kg<sup>-1</sup> at 20 MPa or above 1.0 mol kg<sup>-1</sup> at 40 MPa, the spline surface is unreliable above these molalities.

Ellis ( $\boldsymbol{\theta}$ ) has measured thermal expansions for aqueous CaCl<sub>2</sub> from 323 to 473 K at 0.05-1.0 mol kg<sup>-1</sup> at 2 MPa. The temperature dependence of Ellis' data is in excellent agreement with that calculated from our spline surface at temperatures up to and including 448 K. At 473 K the density values calculated here are 0.5 kg m<sup>-3</sup> higher than the values of Ellis at 0.5 and 1.0 mol kg<sup>-1</sup>. This is approximately 3 times the sum of the estimated errors for both data sets. Romankiw and Chou (7) have measured aqueous CaCl<sub>2</sub> densities using a vibrating tube densimeter at 298 to 318 K. Their results are not compatible with our measurements. The previous measurements at 298.1 K with this instrument compared well with those of Perron, Roux, and Desnoyers (4). Zhang and Frantz (8) determined homogenization temperatures for synthetic CaCl<sub>2</sub>(aq) fluid inclusions at high temperature and pressure. The combination of their data with the previous measurements of Rodnyanskii et al. (9, 10) of the density at the saturation pressure allows the calculation of density as a function of T and P from 300 to 700 °C. Using the equations of Zhang and Frantz (there is a misprint in their eq 21) corrected for the expansion of quartz, we can calculate densities at 326.85 °C for comparison with the present spline surface. The differences are, for m = 0.5

mol kg<sup>-1</sup>, -17 and -24 kg m<sup>-3</sup> at 20 and 40 MPa and, for m =1.0 mol kg<sup>-1</sup>,  $\pm$ 1 and -9 kg m<sup>-3</sup> at 20 and 40 MPa. These differences are within the expected accuracy of the saturation density as estimated by Potter and Clyne (10) ( $\pm$ 10 kg m<sup>-3</sup> from 250 to 300 °C with larger errors above 300 °C).

The data presented here significantly extend the range and quality of volumetric properties of aqueous CaCl<sub>2</sub>. These data allow the calculation of the pressure dependence of free energies, enthalpies, and heat capacities. The data at 600 K are not as accurate as can be obtained from the present instrumentation.

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